

# SWITCHED CAPACITOR VOLTAGE CONVERTERS WITH SHUTDOWN IN SOT PACKAGES

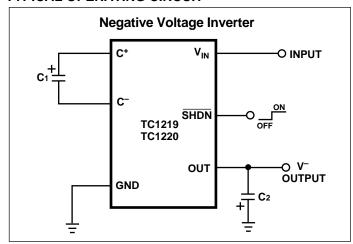
### **FEATURES**

- Charge Pumps in 6-Pin SOT-23A Package
- >95% Voltage Conversion Efficiency
- Voltage Inversion and/or Doubling
- Operates from +2.5V to +5.5V
- Up to 25 mA Output Current
- Only Two External Capacitors Required
- **■** Low Power Consumption
- Power-Saving Shutdown Mode
- TC1220 Compatible with 1.8V Logic Systems

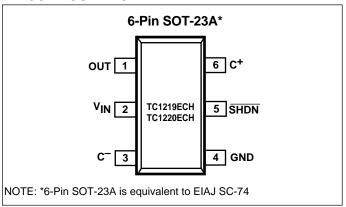
# **APPLICATIONS**

- LCD Panel Bias
- **■** Cellular Phones
- Pagers
- PDAs, Portable Dataloggers
- **■** Battery-Powered Devices

### TYPICAL OPERATING CIRCUIT



# **PIN CONFIGURATION**



### **GENERAL DESCRIPTION**

The TC1219/1220 are CMOS "charge-pump" voltage converters in ultra-small 6-Pin SOT-23A packages. They invert and/or double an input voltage which can range from +2.5V to +5.5V. Conversion efficiency is typically >95%. Switching frequency is 12 KHz for the TC1219, 35 KHz for the TC1220. When the shutdown pin is held at a logic low, the device goes into a very low power mode of operation, consuming less than 1  $\mu A$  of supply current.

External component requirement is only two capacitors for standard voltage inverter applications. With a few additional components a positive doubler can also be built. All other circuitry, including control, oscillator, power MOSFETs are integrated on-chip. Typical supply currents are 60  $\mu$ A (TC1219), 115  $\mu$ A (TC1220).

All devices are available in 6-pin SOT-23A surface mount packages.

# ORDERING INFORMATION

Part No.	Package	Osc. Freq. (KHz)	Temp. Range
TC1219ECH	6-Pin SOT-23	A* 12	- 40°C to +85°C
TC1220ECH	6-Pin SOT-23	A* 35	- 40°C to +85°C

NOTE: \*6-Pin SOT-23A is equivalent to EIAJ SC-74

# **ABSOLUTE MAXIMUM RATINGS\***

Input Voltage (V <sub>IN</sub> to GND)	+6.0V, - 0.3V
Output Voltage (OUT to GND)	6.0V, + 0.3V
Current at OUT Pin	50 mA
Short-Circuit Duration - OUT to GN	ND Indefinite
Operating Temperature Range	40°C to +85°C

Power Dissipation ( $T_A \le 70^{\circ}C$ )	
6-Pin SOT-23A	240 mW
Storage Temperature (Unbiased)	– 65°C to +150°C
Lead Temperature (Soldering, 10	sec)+260°C

<sup>\*</sup>This is a stress rating only and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

**ELECTRICAL CHARACTERISTICS:**  $T_A = -40^{\circ}\text{C}$  to +85°C,  $V_{\text{IN}} = +5\text{V}$ , C1 = C2 = 10  $\mu\text{F}$  (TC1219), C1 = C2 = 3.3 $\mu\text{F}$  (TC1220), unless otherwise noted. Typical values are at  $T_A = +25^{\circ}\text{C}$ .

Symbol	Parameter	Device	Test Conditions	Min	Тур	Max	Unit
I <sub>DD</sub>	Supply Current	TC1219 TC1220		_	60 115	115 325	μА
I <sub>SHDN</sub>	Shutdown Supply Current		SHDN = GND, V <sub>IN</sub> = 5V (Note 2)	_	0.1	1.0	μА
V <sub>MIN</sub>	Minimum Supply Voltage	е	R <sub>LOAD</sub> = 1 KΩ	2.5		_	V
$\overline{V_{MAX}}$	Maximum Supply Voltage		R <sub>LOAD</sub> = 1 KΩ	_		5.5	V
Fosc	Oscillator Frequency	TC1219 TC1220		6 19	12 35	20 56.3	KHz
V <sub>IH</sub>	Shutdown Input Logic High	TC1219 TC1220	$R_{LOAD} = \infty$ $V_{IN} = V_{MIN}$ to 3V $V_{IN} = >3V$ to $V_{MAX}$ $V_{IN} = V_{MIN}$ to $V_{MAX}$	1.5 1.8 1.5	_ _ _	_ _ _	V V
V <sub>IL</sub>	Shutdown Input Logic Low		$V_{IN} = V_{MIN}$ to $V_{MAX}$	_		0.5	V
P <sub>EFF</sub>	Power Efficiency	TC1219 TC1220	R <sub>LOAD</sub> = 1 KΩ	_	96 95	_	%
V <sub>EFF</sub>	Voltage Conversion Efficiency		R <sub>LOAD</sub> = ∞	95	99.9	_	%
R <sub>OUT</sub>	Output Resistance (Note 1)	TC1219/20	$I_{LOAD} = 0.5$ mA to 25mA	_	25	65	Ω

NOTES: 1. Capacitor contribution is approximately 20% of the output impedance [ESR = 1 / pump frequency x capacitance)].

# **PIN DESCRIPTION**

Pin No. (6-Pin SOT-23A)	Symbol	Description
1	OUT	Inverting Charge Pump Output.
2	V <sub>IN</sub>	Positive Power Supply Input.
3	C <sup>-</sup>	Commutation Capacitor Negative Terminal.
4	GND	Ground.
5	SHDN	Shutdown Input (Active Low).
6	C <sup>+</sup>	Commutation Capacitor Positive Terminal.

<sup>2.</sup>  $\ensuremath{V_{\text{IN}}}$  is guaranteed to be disconnected from OUT when the converter is in shutdown.

# **DETAILED DESCRIPTION**

The TC1219/1220 charge pump converters invert the voltage applied to the  $V_{\rm IN}$  pin. Conversion consists of a two-phase operation (Figure 1). During the first phase, switches S2 and S4 are opened and S1 and S3 are closed. During this time, C1 charges to the voltage on  $V_{\rm IN}$  and load current is supplied from C2. During the second phase, S2 and S4 are closed, and S1 and S3 are opened. This action connects C1 across C2, restoring charge to C2.

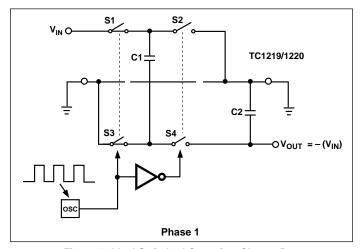


Figure 1. Ideal Switched Capacitor Charge Pump

# APPLICATIONS INFORMATION Output Voltage Considerations

The TC1219/1220 perform voltage conversion but do not provide *regulation*. The output voltage will droop in a linear manner with respect to load current. The value of this equivalent output resistance is approximately  $25\Omega$  nominal at +25°C and  $V_{\text{IN}}$  = +5V.  $V_{\text{OUT}}$  is approximately –5V at light loads, and droops according to the equation below:

$$V_{DROP} = I_{OUT} \times R_{OUT}$$
  
 $V_{OUT} = -(V_{IN} - V_{DROP})$ 

# **Charge Pump Efficiency**

The overall power efficiency of the charge pump is affected by four factors:

- (1) Losses from power consumed by the internal oscillator, switch drive, etc. (which vary with input voltage, temperature and oscillator frequency).
- (2) I<sup>2</sup>R losses due to the on-resistance of the MOSFET switches on-board the charge pump.
- (3) Charge pump capacitor losses due to effective series resistance (ESR).

(4) Losses that occur during charge transfer (from the commutation capacitor to the output capacitor) when a voltage difference between the two capacitors exists.

Most of the conversion losses are due to factors (2) and (3) above. These losses are given by Equation 1(b).

(a) 
$$P_{LOSS(2, 3)} = I_{OUT}^2 \times R_{OUT}$$
  
(b) Where  $R_{OUT} = \left[ \frac{1}{(f_{OSC})(C1)} + 8R_{SWITCH} + 4ESR_{C1} + ESR_{C2} \right]$ 

Equation 1.

The  $1/(f_{OSC})(C1)$  term in Equation 1(b) is the effective output resistance of an ideal switched capacitor circuit (Figures 2a, 2b). The value of  $R_{SWITCH}$  can be approximated at  $0.5\Omega$  for the TC1219/1220.

The remaining losses in the circuit are due to factor (4) above, and are shown in Equation 2. The output voltage ripple is given by Equation 3.

$$P_{LOSS(4)} = \left[ (0.5)(C1)(V_{IN}^2 - V_{OUT}^2) + (0.5)(C2)(V_{RIPPLE}^2 - 2V_{OUT}V_{RIPPLE}) \right]_{X} f_{OSC}$$

Equation 2.

$$V_{RIPPLE} = \frac{I_{OUT}}{(f_{OSC})(C2)} + 2(I_{OUT})(ESR_{C2})$$

Equation 3.

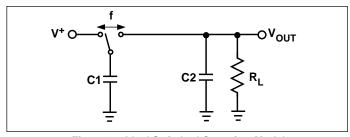


Figure 2a. Ideal Switched Capacitor Model

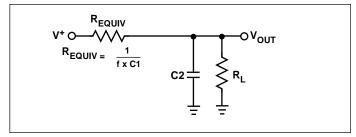


Figure 2b. Equivalent Output Resistance

# **Capacitor Selection**

In order to maintain the lowest output resistance and output ripple voltage, it is recommended that low ESR capacitors be used. Additionally, larger values of C1 will lower the output resistance and larger values of C2 will reduce output ripple. (See Equation 1(b) and Equation 3).

Table 1 shows various values of C1 and the corresponding output resistance values @ +25°C. It assumes a  $0.1\Omega$  ESR<sub>C1</sub> and  $2\Omega$  R<sub>SW</sub>. Table 2 shows the output voltage ripple for various values of C2. The V<sub>RIPPLE</sub> values assume 10mA output load current and  $0.1\Omega$  ESR<sub>C2</sub>.

Table 1. Output Resistance vs. C1 (ESR =  $0.1\Omega$ )

<b>C1(μF)</b>	TC1219 R <sub>OUT</sub> (Ω)	TC1220 R <sub>OUT</sub> (Ω)
1	100	45
3.3	42	25
10	25	19.4
30	19.3	17.5

Table 2. Output Voltage Ripple vs. C2 (ESR =  $0.1\Omega$ )  $I_{OUT}$  10mA

C2 (μF)	TC1219 V <sub>RIPPLE</sub> (mV)	TC1220 V <sub>RIPPLE</sub> (mV)
1	835	286
3.3	254	88
10	85	31
30	29.8	11.5

# Input Supply Bypassing

The  $V_{\rm IN}$  input should be capacitively bypassed to reduce AC impedance and minimize noise effects due to the switching internal to the device. The recommended capacitor depends on the configuration of the TC1219/1220.

# Shutdown Input

The TC1219/1220 is enabled when SHDN is high, and disabled when SHDN is low. This input cannot be allowed to float. (If SHDN is not required, see the TCM828/829 data sheet.) The SHDN input can be only driven to 0.5V above VIN to avoid significant current flows.

# **Voltage Inverter**

The most common application for charge pump devices is the inverter (Figure 3). This application uses two external capacitors: C1 and C2 (plus a power supply bypass capacitor, if necessary). The output is equal to  $-V_{\text{IN}}$  plus any voltage drops due to loading. Refer to Table 1 and Table 2 for capacitor selection.

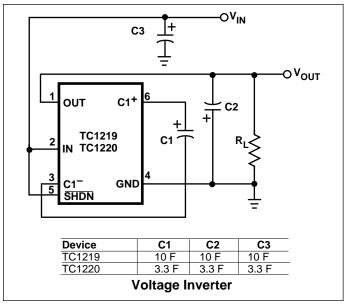


Figure 3. Test Circuit

# **Cascading Devices**

Two or more TC1219/1220 can be cascaded to increase output voltage (Figure 4). If the output is lightly loaded, it will be close to (–  $2 \times V_{\text{IN}}$ ) but will droop at least by  $R_{\text{OUT}}$  of the first device multiplied by the  $I_{\text{Q}}$  of the second. It can be seen that the output resistance rises rapidly for multiple cascaded devices.

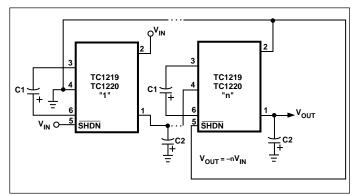


Figure 4. Cascading Multiple Devices to Increase Output Voltage

# **Paralleling Devices**

To reduce the value of  $R_{OUT}$ , multiple TC1219/1220 can be connected in parallel (Figure 5). The output resistance will be reduced by a factor of N where N is the number of TC1219/1220. Each device will require its own pump capacitor (C1), but all devices may share one reservoir capacitor (C2). However, to preserve ripple performance the value of C2 should be scaled according to the number of paralleled TC1219/1220.

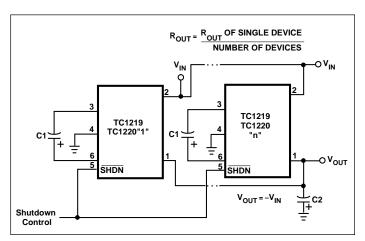


Figure 5. Paralleling Multiple Devices to Reduce Output Resistance

# Voltage Doubler/Inverter

Another common application of the TC1219/1220 is shown in Figure 6. This circuit performs two functions in combination. C1 and C2 form the standard inverter circuit described above. C3 and C4 plus the two diodes form the voltage doubler circuit. C1 and C3 are the pump capacitors and C2 and C4 are the reservoir capacitors. Because both sub-circuits rely on the same switches if either output is loaded, both will droop toward GND. Make sure that the total current drawn from both the outputs does not total more than 40 mA.

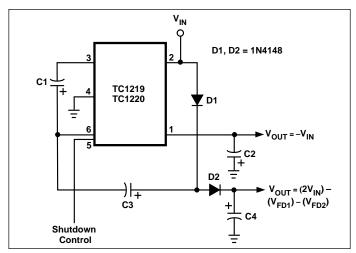


Figure 6. Combined Doubler and Inverter

# **Diode Protection for Heavy Loads**

When heavy loads require the OUT pin to sink large currents being delivered by a positive source, diode protection may be needed. The OUT pin should not be allowed to be pulled above ground. This is accomplished by connecting a Schottky diode (1N5817) as shown in Figure 7.

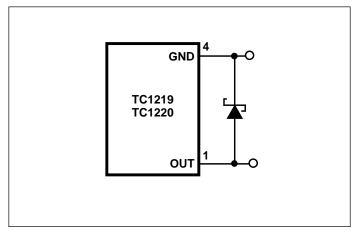


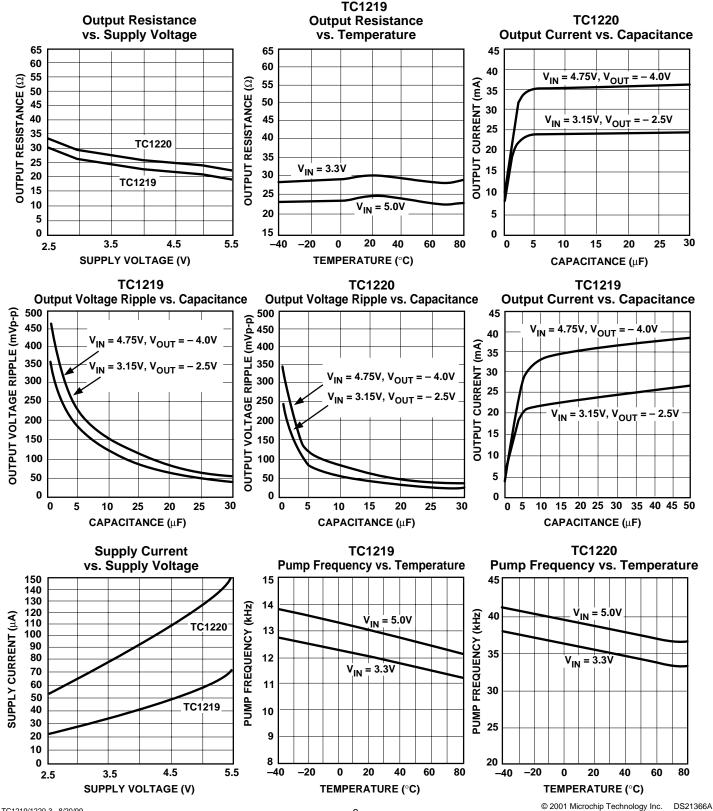
Figure 7. High V-Load Current

# **Layout Considerations**

As with any switching power supply circuit good layout practice is recommended. Mount components as close together as possible to minimize stray inductance and capacitance. Also use a large ground plane to minimize noise leakage into other circuitry.

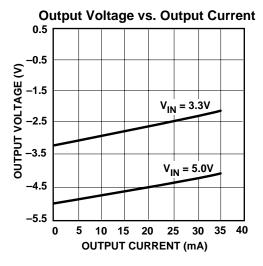
# TYPICAL CHARACTERISTICS

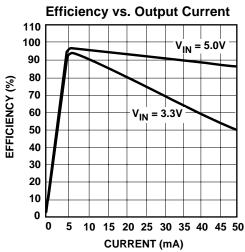
Circuit of Figure 3,  $V_{IN}$  = +5V, C1 = C2 = C3,  $T_A$  = +25°C, unless otherwise noted.



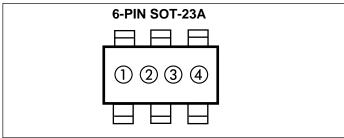
# TYPICAL CHARACTERISTICS (Cont.)

Circuit of Figure 3,  $V_{IN} = +5V$ , C1 = C2 = C3,  $T_A = +25$ °C, unless otherwise noted.





# **MARKING**



Part Numbers and Part Marking

① & ② = part number code + temperature range (two-digit code).

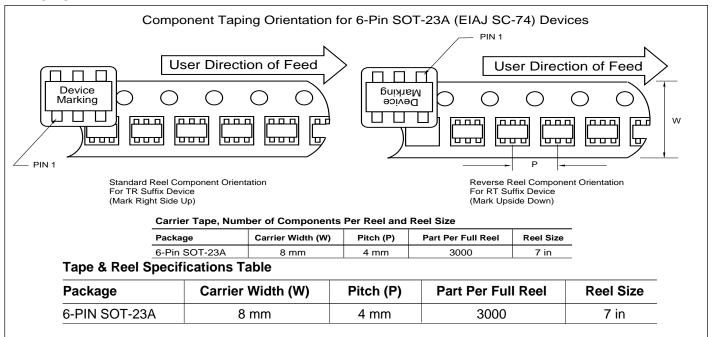
TC1219/1220	Code
TC1219ECH	AM
TC1220ECH	AN

ex: 1219ECH = (A)(M)()

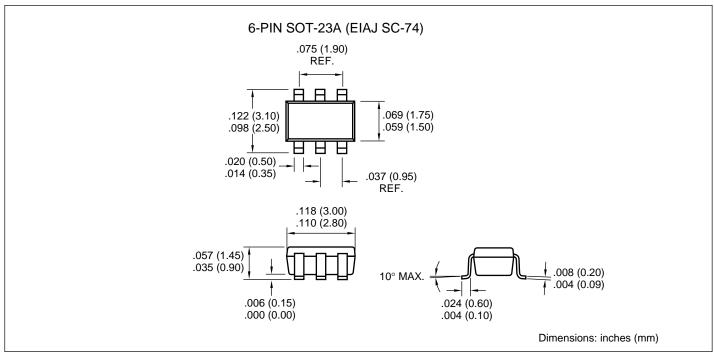
- (3) represents year and quarter code
- 4 represents lot ID number

# TC1219 TC1220

# **TAPING FORM**



### **PACKAGING INFORMATION**





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