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EVALUATION KIT AVAILABLE

# High-Efficiency Step-Up Converters with Reverse Battery Protection in SOT23-6

## **General Description**

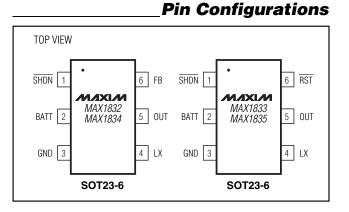
**Applications** 

The MAX1832–MAX1835 are high-efficiency step-up converters with complete reverse battery protection that protects the device and the load when the battery is reversed. They feature a built-in synchronous rectifier, which allows for over 90% efficiency and reduces size and cost by eliminating the need for an external Schottky diode.

These step-up converters operate from a +1.5V to +5.5V input voltage range and deliver up to 150mA of load current. The MAX1833/MAX1835 have a fixed +3.3V output, and the MAX1832/MAX1834 have adjustable outputs from +2V to +5.5V. In shutdown, the MAX1832/MAX1833 connect the battery input to the voltage output, allowing the input battery to be used as a backup or real-time clock supply when the converter is off (see *Selector Guide*).

The MAX1832–MAX1835 are available in a miniature 6pin SOT23 package. The MAX1832EVKIT is available to shorten the design cycle.

> Medical Diagnostic Equipment Pagers Hand-Held Instruments Remote Wireless Transmitters Digital Cameras Cordless Phones Battery Backup PC Cards Local 3.3V or 5V Supply



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### Features

- Reverse Battery Protection for DC-DC Converter and Load
- Up to 90% Efficiency
- No External Diode or FETs Needed
- Internal Synchronous Rectifier
- 4µA Quiescent Current
- <1µA Shutdown Supply Current</p>
- ♦ +1.5V to +5.5V Input Voltage Range
- ♦ Accurate SHDN Threshold for Low-Battery Cutoff
- BATT Connected to OUT in Shutdown for Backup Power (MAX1832/MAX1833)
- RST Output (MAX1833/MAX1835)
- Fixed +3.3V Output Voltage (MAX1833/MAX1835)
- Adjustable Output Voltage (MAX1832/MAX1834)
- Up to 150mA Output Current
- Tiny 6-Pin SOT23 Package

### **Ordering Information**

		-	
PART	TEMP. RANGE	PIN- PACKAGE	TOP MARK
MAX1832EUT-T	-40°C to +85°C	6 SOT23-6	AAOT
MAX1833EUT-T	-40°C to +85°C	6 SOT23-6	AAOU
MAX1834EUT-T	-40°C to +85°C	6 SOT23-6	AAOV
MAX1835EUT-T	-40°C to +85°C	6 SOT23-6	AAOW

**Note:** Requires special solder temperature profile described in the Absolute Maximum Ratings.

## **Selector Guide**

PART	OUTPUT VOLTAGE	OUTPUT VOLTAGE IN SHUTDOWN
MAX1832EUT-T	Adjustable	VBATT
MAX1833EUT-T	Fixed 3.3V	VBATT
MAX1834EUT-T	Adjustable	V <sub>BATT</sub> - 0.7V
MAX1835EUT-T	Fixed 3.3V	V <sub>BATT</sub> - 0.7V

### **ABSOLUTE MAXIMUM RATINGS**

BATT, LX to GND	6V to +6V
LX to OUT	
SHDN to GND	
OUT, FB, RST TO GND	
LX Current	1A
Continuous Dower Dissinction (T.	. 70°C)

Operating Temperature Range	40°C to +85°C
Junction Temperature	+150°C
Storage Temperature Range	65°C to +150°C
Lead Temperature (soldering, 10s) (Note 2).	+300°C

Continuous Power Dissipation ( $T_A = +70^{\circ}C$ )

SOT23-6 (derate 9.1mW/°C above +70°C) (Note 1)....727mW

Note 1: Thermal properties are specified with product mounted on PC board with one square-inch of copper area and still air.
 Note 2: This device is constructed using a unique set of packaging techniques that impose a limit on the thermal profile the device can be exposed to during solder attach and rework. This limit permits only the use of the solder profiles recommended in the industry-standard specification, IPC/JEDEC J-STD-020A, paragraph 7.6, Table 3 for the IR/VPR and Convection reflow. Preheating is required. Hand or wave soldering is not allowed.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## **ELECTRICAL CHARACTERISTICS**

 $(V_{\overline{SHDN}} = +1.5V, V_{OUT} = +3.3V, V_{BATT} = +2V, GND = 0, T_A = -40^{\circ}C$  to +85°C. Typical values are at T<sub>A</sub> = +25°C, unless otherwise noted.) (Note 3)

PARAMETER	SYMBOL	CONDITIONS		MIN	ТҮР	MAX	UNITS
Output Range	Vout	MAX1832/MAX1834		2.0		5.5	V
Battery Input Range	VBATT			1.5		5.5	V
			$T_A = +25^{\circ}C$		1.22	1.5	V
Startup Battery Input Voltage	V <sub>SU</sub>	$R_{LOAD} = 2.6 k\Omega$	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$		1.24		
		MAX1833/	$T_A = +25^{\circ}C$	3.225	3.290	3.355	V
Output Voltage	Vout	MAX1835	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	3.208		3.372	
		MAX1832/	$T_A = +25^{\circ}C$	1.208	1.228	1.248	V
FB Trip Voltage	V <sub>FB</sub>	MAX1834	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	1.204		1.252	
		MAX1832/	$T_A = +25^{\circ}C$		3.5	20	
FB Input Bias Current	. 5	MAX1834, V <sub>FB</sub> = +1.3V	$T_A = -40^{\circ}C$ to $+85^{\circ}C$		4.0		nA
N-Channel On-Resistance	R <sub>NCH</sub>	$V_{OUT} = +3.3V$ $I_{LX} = 100mA$	$T_A = +25^{\circ}C$		0.4	1.2	Ω
N-Channel On-Nesistance			$T_A = -40^{\circ}C$ to $+85^{\circ}C$			1.5	
P-Channel On-Resistance	RPCH	$V_{OUT} = +3.3V$ $T_A = +25^{\circ}C$ $I_{LX} = 100mA$ $T_A = -40^{\circ}C$ to $+85^{\circ}C$	$T_A = +25^{\circ}C$		0.5	1.3	Ω
	NPCH				1.6	52	
P-Channel Catch-Diode Voltage		$I_{LX} = 100$ mA, PCH off, $V_{OUT} = +3.5V$ , $V_{FB} = +1.3V$			0.73		V
			$T_A = +25^{\circ}C$	435	525	615	mA
N-Channel Switch Current Limit	IMAX	$V_{OUT} = +3.3V$	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	400		650	
Switch Maximum On-Time	ton			3.5	5	6.5	μs
Synchronous Rectifier Zero-			$T_A = +25^{\circ}C$	2	17	34	mA
Crossing Current		$V_{OUT} = +3.3V$	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	0		39	ШA
Quiescent Current into OUT		$V_{OUT} = +3.5V,$	$T_A = +25^{\circ}C$		2.5	7.0	
(Note 4)		$V_{FB} = +1.3V$	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$			8.0	μA
Shutdown Current into OUT		$V_{OUT} = +3.5V, V_{\overline{SHDN}} = V_{FB} = 0V$			0.05	1	μΑ

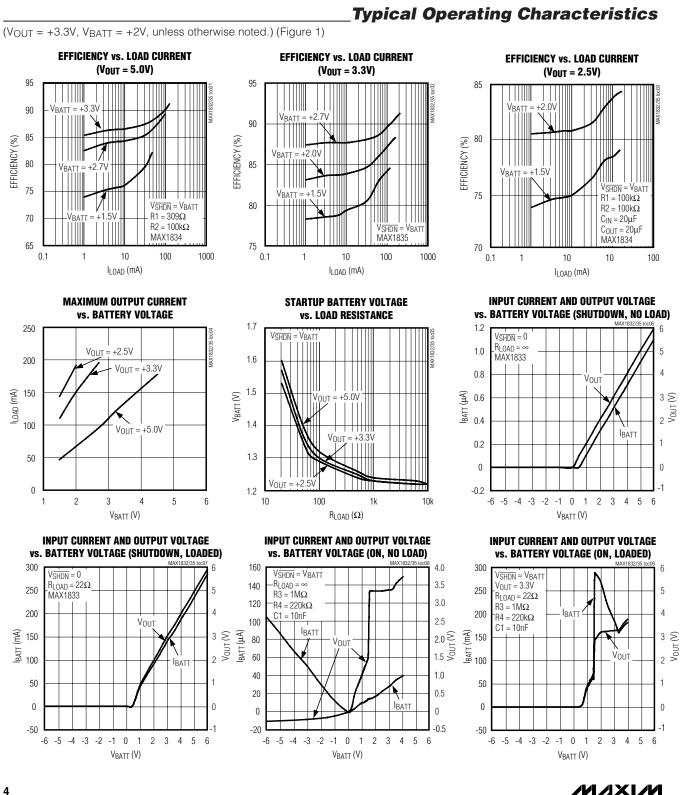
### **ELECTRICAL CHARACTERISTICS (continued)**

(V  $\overline{SHDN}$  = +1.5V, V<sub>OUT</sub> = +3.3V, V<sub>BATT</sub> = +2V, GND = 0, T<sub>A</sub> = -40°C to +85°C. Typical values are at T<sub>A</sub> = +25°C, unless otherwise noted.) (Note 3)

PARAMETER	SYMBOL	CONDITIONS		MIN	ТҮР	MAX	UNITS
Reverse Battery Current into OUT		V <sub>OUT</sub> = 0, V <sub>BATT</sub> = V <sub>SHDN</sub> = V <sub>LX</sub> = -3V			0	10	μΑ
Quiescent Current into BATT		$V_{OUT} = +3.5V,$	$T_A = +25^{\circ}C$		1.8	5.0	uA I
Quiescent Current Into BATT			$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$			6.0	
Shutdown Current into BATT		V <sub>OUT</sub> = +3.5V, \	$I_{BATT} = +2V, V_{\overline{SHDN}} = 0$		0.001	1	μΑ
Reverse Battery Current into BATT		$V_{OUT} = 0$ , $V_{BATT} = V_{\overline{SHDN}} = V_{LX} = -3V$			0.002	10	μΑ
SHDN Logic Low		V <sub>BATT</sub> = +1.5V t	o +5.5V			0.3	V
SHDN Threshold		Rising edge	$T_A = +25^{\circ}C$	1.185	1.228	1.271	- V
SHDN THreshold			$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	1.170		1.286	
SHDN Threshold Hysteresis					0.02		V
SHDN Input Bias Current		V <sub>OUT</sub> = +5.5V, V <sub>SHDN</sub> = +5.5V, T <sub>A</sub> = +25°C			13	100	nA
SHDN Reverse Battery Current		$V_{OUT} = 0$ , $V_{BATT} = V_{\overline{SHDN}} = V_{LX} = -3V$			52	150	μΑ
RST Threshold		MAX1833/ MAX1835.	$T_A = +25^{\circ}C$	2.830	2.980	3.110	v
		falling edge	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	2.800		3.140	v
RST Voltage Low		$I_{\overline{RST}} = 1 \text{mA}, V_{O}$	UT = +2.5V			0.2	V
RST Leakage Current		$V_{\overline{RST}} = +5.5V$	$T_A = +25^{\circ}C$		0.1	100	nA
RST Leakage Current			$T_A = -40^{\circ}C$ to $+85^{\circ}C$		1		
			$T_A = +25^{\circ}C$		1	100	nA
LX Leakage Current		$V_{LX} = +5.5V$	$T_A = -40^{\circ}C$ to $+85^{\circ}C$		100		
LX Reverse Battery Current		$V_{OUT} = 0$ , $V_{BATT} = V_{\overline{SHDN}} = V_{LX} = -3V$			0.001	10	μΑ
Maximum Load Current	ILOAD	$V_{BATT} = +2V, V_{OUT} = +3.3V$			150		mA
Efficiency		$V_{BATT} = +2V$ , $V_{OUT} = +3.3V$ , $I_{LOAD} = 40mA$			90		%

Note 3: All units are 100% production tested at T<sub>A</sub>=+25°C. Limits over the operating temperature range are guaranteed by design and not production tested.

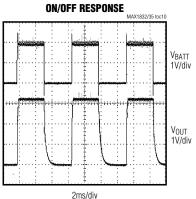
Note 4: Supply current into OUT. This current correlates directly to the actual battery-supply current, but is reduced in value according to the step-up ratio and efficiency.



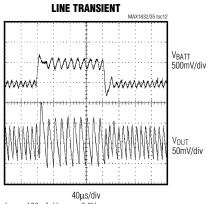
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### **Typical Operating Characteristics (continued)**

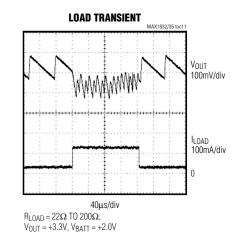
 $(V_{OUT} = +3.3V, V_{BATT} = +2V, unless otherwise noted.)$  (Figure 1)



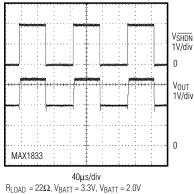
$$\label{eq:VSHDN} \begin{split} & V_{SHDN} = V_{BATT} = 2.0V, \ R_{LOAD} = 22\Omega, \\ & V_{OUT} = 3.3V \end{split}$$



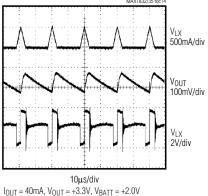
 $I_{OUT} = 100$  mA,  $V_{OUT} = +3.3$ V,  $V_{BATT} = +2.0$ V TO +2.5V



SHUTDOWN RESPONSE







M/IXI/N

## **Pin Description**

Р	IN			
MAX1832 MAX1834	MAX1833 MAX1835	NAME	FUNCTION	
1	1	SHDN	Shutdown. A high logic level turns on the device. When SHDN is low the par and the current into BATT is typically 0.1µA. For the MAX1832/MAX1833, the battery is connected to OUT through an internal PFET and the external indu when SHDN is low. SHDN can be used for low-battery cutoff (1.228V thresh See Low-Battery Cutoff. SHDN has reverse battery protection.	
2	2	BATT	Battery Voltage Connection. BATT has reverse battery protection.	
3	3	GND	Ground	
4	4	LX	Inductor Connection. N-channel MOSFET switch drain and synchronous rectifier P-channel switch drain. LX has reverse battery protection.	
5	5	OUT	Output Voltage. Bootstrapped supply for the device. Output sense point for MAX1833/MAX1835.	
6	—	FB	MAX1832/MAX1834 Feedback Input. Set the output voltage through a resistor-divider network. See Setting the Output Voltage.	
_	6	RST	MAX1833/MAX1835 Power-On Reset Open-Drain Output. RST pulls low when the output is 10% below the regulation point. If not used, connect to GND.	

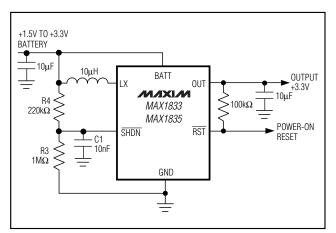


Figure 1a. MAX1833/MAX1835 Typical Operating Circuit

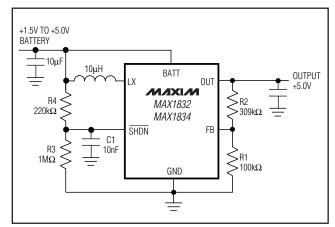


Figure 1b. MAX1832/MAX1834 Typical Operating Circuit

M/IXI/M

### **Detailed Description**

The MAX1832–MAX1835 compact, high-efficiency step-up converters feature 4µA quiescent supply current to ensure the highest possible efficiency over a wide load range. With a minimum +1.5V input voltage, these devices are well suited for applications with two alkaline cells, two nickel-metal-hydride (NiMH) cells, or one lithium ion (Li+) cell. For the MAX1832 and MAX1833, the battery is connected to OUT through the inductor and an internal PFET when SHDN is low. This allows the input battery to be used as a backup or real-time clock supply when the converter is off by eliminating the voltage drop across the PFET body diode.

The MAX1832–MAX1835 are ideal for low-power applications where ultra-small size is critical. These devices feature built-in synchronous rectification that significantly improves efficiency and reduces size and cost by eliminating the need for an external Schottky diode. Furthermore, these devices are the industry's first boost regulators to offer complete reverse battery protection. This proprietary design protects the battery, IC, and the circuitry powered by the IC in the event the input batteries are connected backwards.

#### **Control Scheme**

A current-limited control scheme is a key feature of the MAX1832–MAX1835. This scheme provides ultra-low quiescent current and high efficiency over a wide output current range. There is no oscillator. The inductor current is limited by the 0.5A N-channel current limit or by the 5µs switch maximum on-time. Following each on-cycle, the inductor current must ramp to zero before another cycle may start. When the error comparator senses that the output has fallen below the regulation threshold, another cycle begins.

An internal synchronous rectifier eliminates the need for an external Schottky diode reducing cost and board space. While the inductor discharges, the P-channel MOSFET turns on and shunts the MOSFET body diode. As a result, the rectifier voltage drop is significantly reduced, improving efficiency without adding external components.

#### **Reverse Battery Protection**

The MAX1832–MAX1835 have a unique proprietary design that protects the battery, IC, and circuitry powered by the IC in the event that the input batteries are connected backwards. When the batteries are connected correctly, the reverse battery protection N-channel MOSFET is on and the device operates normally. When the batteries are connected backwards, the

reverse battery protection N-channel MOSFET opens, protecting the device and load (Figures 2 and 3). Previously, this level of protection required additional circuitry and reduced efficiency due to added components in the battery current path.

### **Applications Information**

#### Shutdown

When SHDN is low, the device is off and no current is drawn from the battery. When SHDN is high, the device is on. If SHDN is driven from a logic-level output, the logic high (on) level should be referenced to  $V_{OUT}$  to avoid intermittent turn on. If SHDN is not used at all, connect it to OUT. With SHDN connected to OUT, the MAX1834/MAX1835 startup voltage (1.65V) is slightly higher, due to the voltage across the PFET body diode. The SHDN pin has reverse battery protection.

In shutdown, the MAX1832/MAX1833 connect the battery input to the output through the inductor and the internal synchronous rectifier PFET. This allows the input battery (rather than a separate backup battery) to provide backup power for devices such as an idled microcontroller, SRAM, or real-time clock, without the usual diode forward drop. If the output has a residual voltage during shutdown, a small amount of energy will be transfered from the output back to the input immediately after shutdown. This energy transfer may cause a slight momemntary "bump" in the input voltage. The magnitude and duration of the input bump are related to the ratio of CIN and COUT and the ability of the input to sink current. With battery input sources, the bump will be negligible, but with power-supply inputs (that typically cannot sink current), the bump may be 100s of mV.

In shutdown, the MAX1834/MAX1835 do not turn on the internal PFET and thus do not have an output-to-input current path in shutdown. This allows a separate back-up battery, such as a Li+ cell, to be diode-connected at the output, without leakage current flowing to the input. The MAX1834/MAX1835 still have the typical input-to-output current path from the battery to the output, through the PFET body diode, in shutdown.

#### Low-Battery Cutoff

The SHDN trip threshold of the MAX1832–MAX1835 can be used as a voltage detector, with a resistordivider, to power down the IC when the battery voltage falls to a set level (Figure 1). The SHDN trip threshold is 1.228V. To use a resistor-divider to set the shutdown voltage, select a value for R3 in the 100k $\Omega$  to 1M $\Omega$ 



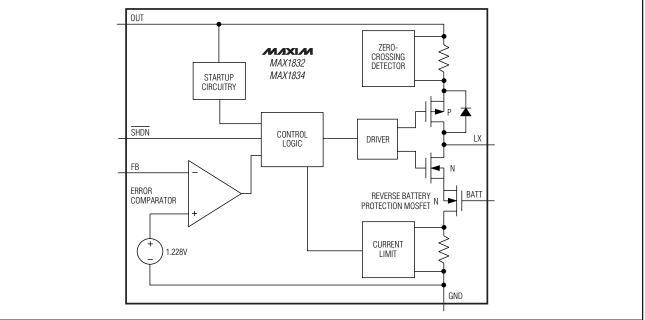


Figure 2. MAX1832/MAX1834 Simplified Functional Diagram

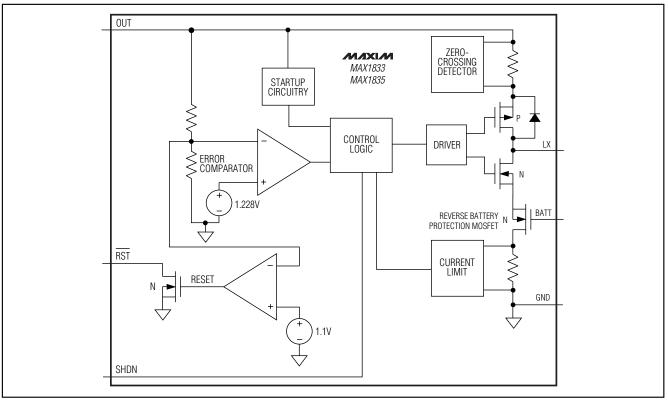


Figure 3. MAX1833/MAX1835 Simplified Functional Diagram

range to minimize battery drain. Calcuate R4 as follows:

#### $R4 = R3 \times (VOFF / VSHDN - 1)$

VOFF is the battery voltage at which the part will shut down and V<sub>SHDN</sub> = 1.228V. Note that input ripple can sometimes cause false shutdowns. To minimize the effect of ripple, connect a low-value capacitor (C1) from SHDN to GND to filter out input noise. Select a C1 value such that the R4 × C1 time constant is above 2ms.

#### **Power-On Reset**

The MAX1833/MAX1835 provide a power-on reset output (RST). A 100k $\Omega$  to 1M $\Omega$  pullup resistor from RST to OUT provides a logic control signal. This open-drain output pulls low when the output is 10% below its regulation point. If not used, connect it to GND.

#### **Setting the Output Voltage**

The output voltage of the MAX1832/MAX1834 is adjustable from +2V to +5.5V, using external resistors R1 and R2 (Figure 1b). Since FB leakage is 20nA (max), select feedback resistor R1 to be 100k $\Omega$  to 1M $\Omega$ . Calculate R2 as follows:

$$R2 = R1 \left( \frac{V_{OUT}}{V_{FB}} - 1 \right)$$

where  $V_{FB} = 1.228V$ .

#### **Inductor Selection**

The control scheme of the MAX1832–MAX1835 permits flexibility in choosing an inductor. A 10µH inductor performs well for most applications, but values from 4.7µH to 100µH may also be used. Small inductance values typically offer smaller physical size. Large inductance values minimize output ripple but reduce output power. Output power is reduced when the inductance is large enough to prevent the maximum current limit (525mA) from being reached before the maximum on-time (5µs) expires.

For maximum output current, choose L such that:

$$\frac{V_{BATT(MAX)}(1\mu s)}{0.525A} < L < \frac{V_{BATT(MIN)}(5\mu s)}{0.525A}$$
$$I_{OUT(MAX)} = \frac{0.525A}{2} \times \frac{V_{BATT(MIN)} - \frac{0.525A}{2} \left(R_{NCH} + R_{IND}\right)}{V_{OUT}}$$

where  $R_{IND}$  is the inductor series resistance, and  $R_{NCH}$  is the  $R_{DS(ON)}$  of the N-channel MOSFET (0.4  $\Omega$  typ).

# Table 1. Suggested Inductors and Suppliers

MANUFACTURER	INDUCTOR	PHONE
Coilcraft	DS1608C-103 DO1606T-103	847-639-6400
Sumida	CDRH4D18-100 CR43-100	847-956-0666
Murata	LQH4N100K	814-237-1431

# Table 2. Suggested Surface-MountCapacitors and Manufacturers

VALUE (µF)	DESCRIPTION	MANU- FACTURER	PHONE
4.7 to	594/595 D- series tantalum	Sprague	603-224-1961
47	TAJ, TPS- series tantalum	AVX	803-946-0690
4.7 to 10	X7R ceramic	TDK	847-390-4373
4.7 to 22	X7R ceramic	Taiyo Yuden	408-573-4150

#### **Capacitor Selection**

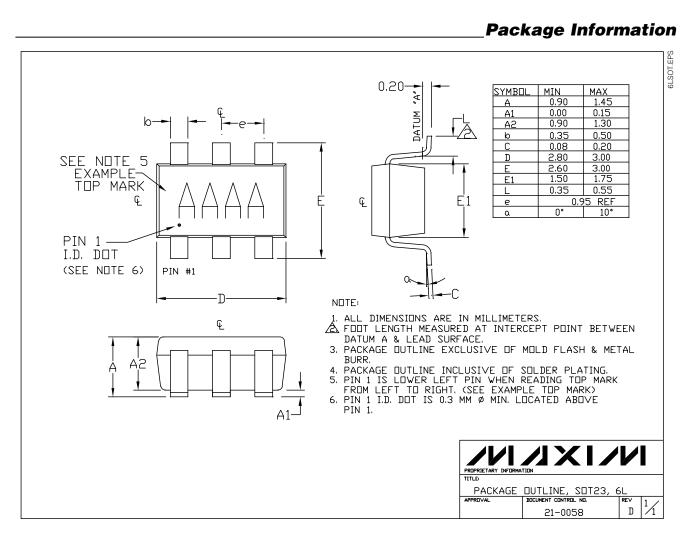
Choose an output capacitor to achieve the desired output ripple percentage.

$$C_{OUT} > \frac{0.5 \times L \times 0.525 A^2}{r\% \times V_{OUT}^2}$$

where r is the desired output ripple in %. A  $10\mu$ F ceramic capacitor is a good starting value. The input capacitor reduces the peak current drawn from the battery and can be the same value as the input capacitor. A larger input capacitor can be used to further reduce ripple and improve efficiency.

#### **PC Board Layout and Grounding**

Careful printed circuit layout is important for minimizing ground bounce and noise. Keep the IC's GND pin and the ground leads of the input and output filter capacitors less than 0.2in (5mm) apart. In addition, keep all connections to the FB and LX pins as short as possible. In particular, when using external feedback resistors,



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