## Radiation Hardened, Dual, High Speed Low Power, Video Closed Loop Buffer

The HS-1212RH is a dual closed loop buffer featuring user programmable gain and high speed performance. Manufactured on Intersil's proprietary complementary bipolar UHF-1 (DI bonded wafer) process, this device offers wide -3 dB bandwidth of 340 MHz , very fast slew rate, excellent gain flatness and high output current. These devices are QML approved and are processed and screened in full compliance with MIL-PRF-38535.
A unique feature of the pinout allows the user to select a voltage gain of $+1,-1$, or +2 , without the use of any external components. Gain selection is accomplished via connections to the inputs, as described in the "Application Information" section. The result is a more flexible product, fewer part types in inventory, and more efficient use of board space.

Compatibility with existing op amp pinouts provides flexibility to upgrade low gain amplifiers, while decreasing component count. Unlike most buffers, the standard pinout provides an upgrade path should a higher closed loop gain be needed at a future date.

Specifications for Rad Hard QML devices are controlled by the Defense Supply Center in Columbus (DSCC). The SMD numbers listed here must be used when ordering.

Detailed Electrical Specifications for these devices are contained in SMD 5962-96831. A "hot-link" is provided on our homepage for downloading. www.intersil.com/spacedefense/space.asp

## Ordering Information

| ORDERING NUMBER | INTERNAL <br> MKT. NUMBER | TEMP. RANGE <br> ( $\left.{ }^{\circ} \mathrm{C}\right)$ |
| :--- | :--- | :---: |
| 5962F9683101VPA | HS7-1212RH-Q | -55 to 125 |
| 5962F9683101VPC | HS7B-1212RH-Q | -55 to 125 |

## Features

- Electrically Screened to SMD \# 5962-96831
- QML Qualified per MIL-PRF-38535 Requirements
- MIL-PRF-38535 Class V Compliant
- User Programmable For Closed-Loop Gains of $+1,-1$ or +2 Without Use of External Resistors
- Standard Operational Amplifier Pinout
- Low Supply Current $5.9 \mathrm{~mA} / \mathrm{Op}$ Amp (Typ)
- Excellent Gain Accuracy . . . . . . . . . . . . . . 0.99V/V (Typ)
- Wide -3dB Bandwidth. . . . . . . . . . . . . . . . . . 340MHz (Typ)
- Fast Slew Rate . . . . . . . . . . . . . . . . . . . . . .1155V/ $\mu \mathrm{s}$ (Typ)
- High Input Impedance . . . . . . . . . . . . . . . . . . . 1M 1 (Typ)
- Excellent Gain Flatness (to 50 MHz ) . . . . . . $\pm 0.02 \mathrm{~dB}$ (Typ)
- Fast Overdrive Recovery . . . . . . . . . . . . . . . . <10ns (Typ)
- Total Gamma Dose.

300kRAD(Si)

- Latch Up None (DI Technology)


## Applications

- Flash A/D Driver
- Video Switching and Routing
- Pulse and Video Amplifiers
- Wideband Amplifiers
- RF/IF Signal Processing
- Imaging Systems


## Pinout



## Application Information

## HS-1212RH Advantages

The HS-1212RH features a novel design which allows the user to select from three closed loop gains, without any external components. The result is a more flexible product, fewer part types in inventory, and more efficient use of board space. Implementing a dual, gain of 2 , cable driver with this IC eliminates the four gain setting resistors, which frees up board space for termination resistors.

Like most newer high performance amplifiers, the HS-1212RH is a current feedback amplifier (CFA). CFAs offer high bandwidth and slew rate at low supply currents, but can be difficult to use because of their sensitivity to feedback capacitance and parasitics on the inverting input (summing node). The HS-1212RH eliminates these concerns by bringing the gain setting resistors on-chip. This yields the optimum placement and value of the feedback resistor, while minimizing feedback and summing node parasitics. Because there is no access to the summing node, the PCB parasitics do not impact performance at gains of +2 or -1 (see "Unity Gain Considerations" for discussion of parasitic impact on unity gain performance).

The HS-1212RH's closed loop gain implementation provides better gain accuracy, lower offset and output impedance, and better distortion compared with open loop buffers.

## Closed Loop Gain Selection

This "buffer" operates in closed loop gains of $-1,+1$, or +2 , with gain selection accomplished via connections to the inputs Applying the input signal to $+\mathbb{I N}$ and floating -IN selects a gain of +1 (see next section for layout caveats), while grounding -IN selects a gain of +2 . A gain of -1 is obtained by applying the input signal to -IN with +IN grounded through a $50 \Omega$ resistor.

The table below summarizes these connections:

| GAIN <br> (ACL) | CONNECTIONS |  |
| :---: | :---: | :---: |
|  | +INPUT | -INPUT |
| -1 | $50 \Omega$ to GND | Input |
| +1 | Input | NC (Floating) |
| +2 | Input | GND |

## Unity Gain Considerations

Unity gain selection is accomplished by floating the -Input of the HS-1212RH. Anything that tends to short the -Input to GND, such as stray capacitance at high frequencies, will cause the amplifier gain to increase toward a gain of +2 . The result is excessive high frequency peaking, and possible instability. Even the minimal amount of capacitance associated with attaching the -Input lead to the PCB results in approximately 6 dB of gain peaking. At a minimum this requires due care to ensure the minimum capacitance at the -Input connection.

Table 1 lists five alternate methods for configuring the HS-1212RH as a unity gain buffer, and the corresponding performance. The implementations vary in complexity and involve performance trade-offs. The easiest approach to implement is simply shorting the two input pins together, and applying the input signal to this common node. The amplifier bandwidth decreases from 430 MHz to 280 MHz , but excellent gain flatness is the benefit. A drawback to this approach is that the amplifier input noise voltage and input offset voltage terms see a gain of +2 , resulting in higher noise and output offset voltages. Alternately, a 100pF capacitor between the inputs shorts them only at high frequencies, which prevents the increased output offset voltage but delivers less gain flatness.

Another straightforward approach is to add a $620 \Omega$ resistor in series with the amplifier's positive input. This resistor and the HS-1212RH input capacitance form a low pass filter which rolls off the signal bandwidth before gain peaking occurs. This configuration was employed to obtain the data sheet AC and transient parameters for a gain of +1 .

## Pulse Overshoot

The HS-1212RH utilizes a quasi-complementary output stage to achieve high output current while minimizing quiescent supply current. In this approach, a composite device replaces the traditional PNP pulldown transistor. The composite device switches modes after crossing 0 V , resulting in added distortion for signals swinging below ground, and an increased overshoot on the negative portion of the output waveform (see Figure 6,
Figure 9, and Figure 12). This overshoot isn't present for small bipolar signals (see Figure 4, Figure 7, and Figure 10) or large positive signals (see Figure 5, Figure 8 and Figure 11).

## PC Board Layout

This amplifier's frequency response depends greatly on the care taken in designing the PC board (PCB). The use of low inductance components such as chip resistors and chip capacitors is strongly recommended, while a solid ground plane is a must!
Attention should be given to decoupling the power supplies. A large value $(10 \mu \mathrm{~F})$ tantalum in parallel with a small value $(0.1 \mu \mathrm{~F})$ chip capacitor works well in most cases.

TABLE 1. UNITY GAIN PERFORMANCE FOR VARIOUS IMPLEMENTATIONS

| APPROACH | PEAKING (dB) | BW (MHz) | $\pm 0.1 \mathrm{~dB}$ GAIN FLATNESS (MHz) |
| :--- | :---: | :---: | :---: |
| Remove -IN Pin | 4.5 | 430 | 21 |
| $+R_{S}=620 \Omega$ | 0 | 220 | 27 |
| $+R_{S}=620 \Omega$ and Remove -IN Pin | 0.5 | 215 | 15 |
| Short + IN to -IN (e.g., Pins 2 and 3) | 0.6 | 280 | 70 |
| 100 pF Capacitor Between + IN and -IN | 0.7 | 290 | 40 |

Terminated microstrip signal lines are recommended at the input and output of the device. Capacitance directly on the output must be minimized, or isolated as discussed in the next section.

An example of a good high frequency layout is the Evaluation Board shown in Figure 3.

## Driving Capacitive Loads

Capacitive loads, such as an A/D input, or an improperly terminated transmission line will degrade the amplifier's phase margin resulting in frequency response peaking and possible oscillations. In most cases, the oscillation can be avoided by placing a resistor $\left(R_{\mathrm{S}}\right)$ in series with the output prior to the capacitance.

Figure 1 details starting points for the selection of this resistor. The points on the curve indicate the $R_{S}$ and $C_{L}$ combinations for the optimum bandwidth, stability, and settling time, but experimental fine tuning is recommended. Picking a point above or to the right of the curve yields an overdamped response, while points below or left of the curve indicate areas of underdamped performance.
$R_{S}$ and $C_{L}$ form a low pass network at the output, thus limiting system bandwidth well below the amplifier bandwidth of 350 MHz . By decreasing $R_{S}$ as $C_{L}$ increases (as illustrated in the curves), the maximum bandwidth is obtained without sacrificing stability. In spite of this, bandwidth decreases as the load capacitance increases.


FIGURE 1. RECOMMENDED SERIES RESISTOR vs LOAD CAPACITANCE

## Evaluation Board

The performance of the HS-1212RH may be evaluated using the HA5023 Evaluation Board, slightly modified as follows:

1. Remove the two feedback resistors, and leave the connections open.
2. a. For $A_{V}=+1$ evaluation, remove the gain setting resistors $\left(R_{1}\right)$, and leave pins 2 and 6 floating.
b. For $A_{V}=+2$, replace the gain setting resistors $\left(R_{1}\right)$ with $0 \Omega$ resistors to GND.
The modified schematic for amplifier 1, and the board layout are shown in Figures 2 and 3.

To order evaluation boards (part number HA5023EVAL), please contact your local sales office.


FIGURE 2. MODIFIED EVALUATION BOARD SCHEMATIC


FIGURE 3A. TOP LAYOUT


FIGURE 3B. BOTTOM LAYOUT

FIGURE 3. EVALUATION BOARD LAYOUT
Typical Performance Curves $\mathrm{V}_{\text {SUPPLY }}= \pm 5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}}=100 \Omega$, Unless Otherwise Specified


FIGURE 4. SMALL SIGNAL PULSE RESPONSE


FIGURE 6. LARGE SIGNAL BIPOLAR PULSE RESPONSE


FIGURE 5. LARGE SIGNAL POSITIVE PULSE RESPONSE


FIGURE 7. SMALL SIGNAL PULSE RESPONSE

Typical Performance Curves $\mathrm{V}_{\text {SUPPLY }}= \pm 5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}}=100 \Omega$, Unless Otherwise Specified (Continued)


TIME (5ns/DIV.)

FIGURE 8. LARGE SIGNAL POSITIVE PULSE RESPONSE


FIGURE 10. SMALL SIGNAL PULSE RESPONSE


FIGURE 12. LARGE SIGNAL BIPOLAR PULSE RESPONSE


FIGURE 9. LARGE SIGNAL BIPOLAR PULSE RESPONSE


FIGURE 11. LARGE SIGNAL POSITIVE PULSE RESPONSE


FIGURE 13. FREQUENCY RESPONSE

Typical Performance Curves $\mathrm{V}_{\text {SUPPLY }}= \pm 5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}}=100 \Omega$, Unless Otherwise Specified (Continued)


FIGURE 14. FULL POWER BANDWIDTH


FIGURE 16. REVERSE ISOLATION


FIGURE 18. 2nd HARMONIC DISTORTION vs Pout


FIGURE 15. GAIN FLATNESS


FIGURE 17. ALL HOSTILE CROSSTALK


FIGURE 19. 3rd HARMONIC DISTORTION vs Pout

Typical Performance Curves $\mathrm{V}_{\text {SUPPLY }}= \pm 5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}}=100 \Omega$, Unless Otherwise Speciied (Continued)


FIGURE 20. SETTLING RESPONSE


FIGURE 21. INPUT NOISE CHARACTERISTICS


FIGURE 22. OUTPUT VOLTAGE vs TEMPERATURE

## Burn-In Circuit



NOTES:

1. $R 1=1 \mathrm{k} \Omega, \pm 5 \%$ (Per Socket).
2. $\mathrm{C} 1=\mathrm{C} 2=0.01 \mu \mathrm{~F}$ (Per Socket) or $0.1 \mu \mathrm{~F}$ (Per Row) Minimum.
3. $\mathrm{D} 1=\mathrm{D} 2=1 \mathrm{~N} 4002$ or Equivalent (Per Board).
4. $\mathrm{D} 3=\mathrm{D} 4=1 \mathrm{~N} 4002$ or Equivalent (Per Socket).
5. $|(-\mathrm{V})|+|(+\mathrm{V})|=11 \mathrm{~V} \pm 1.0 \mathrm{~V}$.
6. $10 \mathrm{~mA}<\left|\mathrm{ICC}, \mathrm{I}_{\mathrm{EE}}\right|<16 \mathrm{~mA}$.
7. $-50 \mathrm{mV}<\mathrm{V}_{\text {OUT }}<+50 \mathrm{mV}$.

## Irradiation Circuit

HS-1212RH CERDIP


NOTES:
8. $R 1=1 \mathrm{k} \Omega, \pm 5 \%$
9. $\mathrm{C} 1=0.01 \mu \mathrm{~F}$
10. $\mathrm{V}+=+5.0 \mathrm{~V} \pm 0.5 \mathrm{~V}$
11. $\mathrm{V}-=-5.0 \mathrm{~V} \pm 0.5 \mathrm{~V}$

## Die Characteristics

DIE DIMENSIONS:
69 mils x 92 mils $\times 19$ mils
$1750 \mu \mathrm{~m} \times 2330 \mu \mathrm{~m} \times 483 \mu \mathrm{~m}$
INTERFACE MATERIALS:

## Glassivation:

Type: Nitride
Thickness: $4 \mathrm{k} \AA \pm 0.5 \mathrm{k} \AA$

## Top Metallization:

Type: Metal 1: $\operatorname{AICu}(2 \%) / T i W$
Thickness: Metal 1: 8k $\AA \pm 0.4 \mathrm{k} \AA$
Type: Metal 2: AICu(2\%)
Thickness: Metal 2: 16k $\AA 0.8 \mathrm{k} \AA$

## Substrate:

UHF-1X, Bonded Wafer, DI

## Backside Finish:

Silicon

## ASSEMBLY RELATED INFORMATION:

Substrate Potential (Powered Up):
Floating (Recommend Connection to V-)

## ADDITIONAL INFORMATION:

## Transistor Count:

180

Metallization Mask Layout


All Intersil semiconductor products are manufactured, assembled and tested under ISO9000 quality systems certification.

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